

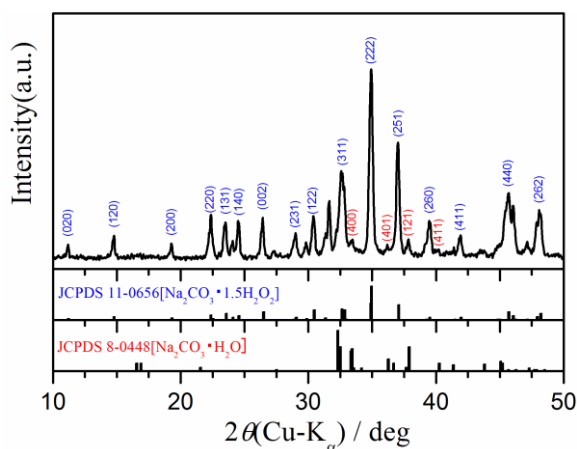
# Multistep Kinetic Behavior of the Thermal Decomposition of Granular Sodium Percarbonate: Hindrance Effect of the Outer Surface Layer

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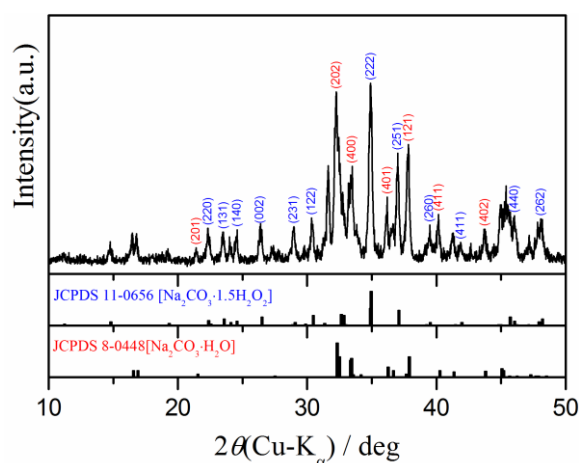
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## S1. Sample Characterization

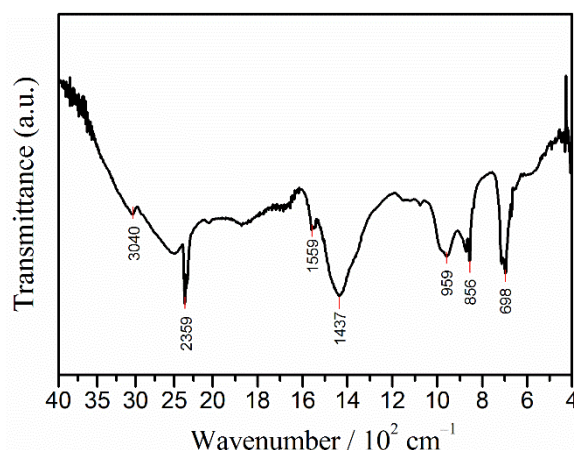
The major XRD peaks of the as-received SPC granules (Figure S1) were indexed to those of  $\text{Na}_2\text{CO}_3 \cdot 1.5\text{H}_2\text{O}_2$  (orthorhombic, S.G.: *Cmca*,  $a = 6.7138 \text{ \AA}$ ,  $b = 15.7407 \text{ \AA}$ ,  $c = 9.1732 \text{ \AA}$ , JCPDS 11-0656),<sup>S1</sup> but some minor peaks were also detected. After exposing the SPC granules in air for several months, those minor peaks substantially grew (Figure S2) and were clearly assigned to those of  $\text{Na}_2\text{CO}_3 \cdot \text{H}_2\text{O}$  (orthorhombic, S.G.: *Pca21*,  $a = 10.72 \text{ \AA}$ ,  $b = 5.249 \text{ \AA}$ ,  $c = 6.469 \text{ \AA}$ , JCPDS 8-0448). The minor phase of  $\text{Na}_2\text{CO}_3 \cdot \text{H}_2\text{O}$  in the as-received SPC granules was likely generated during the granulation process via the decomposition of SPC and is a component in the outer surface layer of the granules. The FT-IR spectrum of the as-received SPC granules (Figure S3) was in agreement with that reported previously for SPC crystalline particles and included IR absorption peaks attributed to  $\text{H}_2\text{O}_2$  and  $\text{CO}_3^{2-}$ : symmetric O–H stretching ( $3040 \text{ cm}^{-1}$ ); asymmetric O–H stretching ( $2359 \text{ cm}^{-1}$ );  $\text{H}_2\text{O}_2$  deformation ( $1559 \text{ cm}^{-1}$ ); O–O stretching ( $856 \text{ cm}^{-1}$ );  $\text{H}_2\text{O}_2$  torsion ( $959 \text{ cm}^{-1}$ ); and internal  $\text{CO}_3^{2-}$  modes ( $1437$  and  $698 \text{ cm}^{-1}$ ).<sup>S2,S3</sup>



**Figure S1.** XRD pattern of the as-received SPC granules.



**Figure S2.** XRD pattern of the partially hydrated SPC granules.



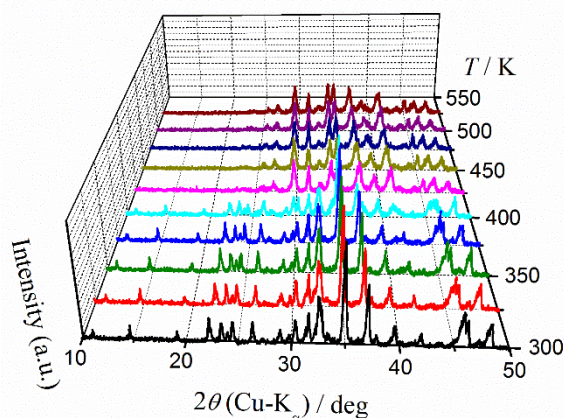
**Figure S3.** FT-IR spectrum of the as-received SPC granules.

## S2. Overview of the Thermal Decomposition Process

Upon heating the crushed SPC granules according to a stepwise isothermal heating program (300 to 525 K) in flowing  $\text{N}_2$ , the XRD pattern for  $\text{Na}_2\text{CO}_3 \cdot 1.5\text{H}_2\text{O}_2$  changed to  $\text{Na}_2\text{CO}_3$  (monoclinic b axis, S.G.: *C2/m*,  $a = 8.907 \text{ \AA}$ ,  $b = 5.239 \text{ \AA}$ ,  $c = 6.043 \text{ \AA}$ ,  $\beta = 101.3^\circ$ , JCPDS

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19-1130) in the temperature range from 375 to 425 K (Figure S4). No other crystalline phases of intermediate compounds were detected during the thermal decomposition.

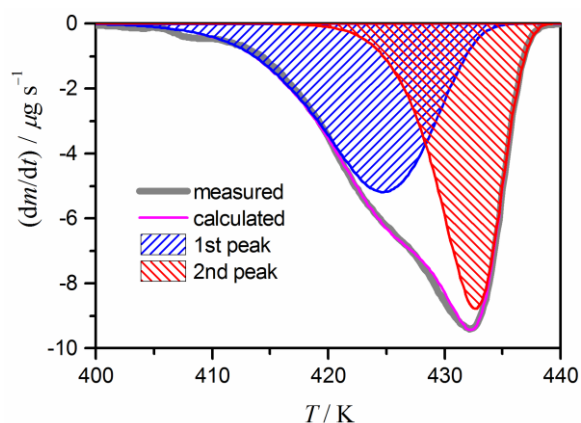


**Figure S4.** Changes in the XRD pattern of crushed SPC granules during stepwise isothermal heating in flowing  $N_2$  ( $100 \text{ cm}^3 \text{ min}^{-1}$ ).

### S3. Kinetic Analysis using a Mathematical Peak Deconvolution Procedure

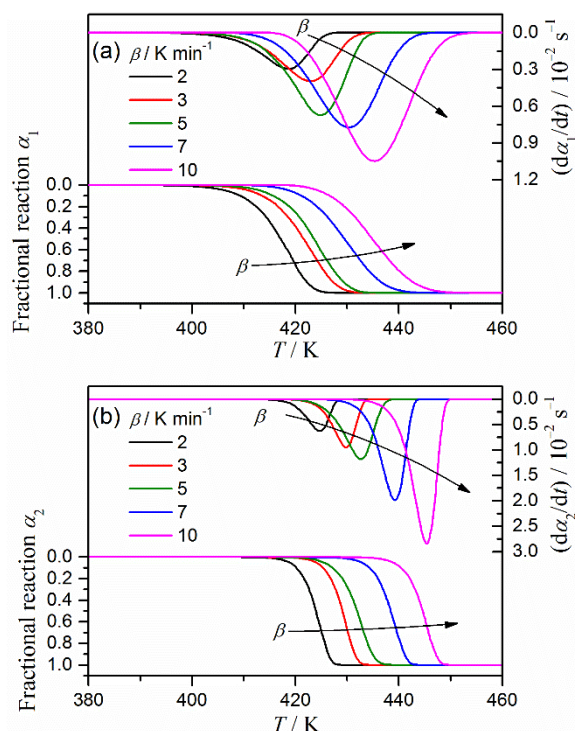
The DTG curve for the thermal decomposition of SPC granules recorded under linear nonisothermal conditions (Figure S5) was separated into two partially overlapping peaks with satisfactory fit using Weibull functions.<sup>S4-S6</sup>

$$y = \left[ a_0 \left( \frac{a_3 - 1}{a_3} \right)^{\frac{1-a_3}{a_3}} \left\{ \frac{x - a_1}{a_2} + \left( \frac{a_3 - 1}{a_3} \right)^{\frac{1}{a_3}} \right\}^{a_3 - 1} \right] \exp \left[ - \left\{ \frac{x - a_1}{a_2} + \left( \frac{a_3 - 1}{a_3} \right)^{\frac{1}{a_3}} \right\}^{a_3} + \frac{a_3 - 1}{a_3} \right] \quad (\text{S1})$$



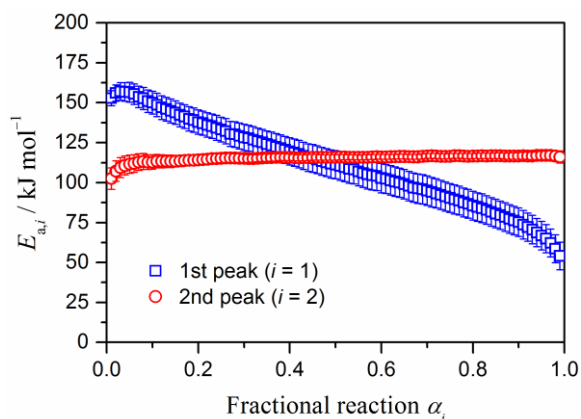
**Figure S5.** Typical mathematical deconvolution of the DTG curve for the thermal decomposition of SPC granules at  $\beta = 5 \text{ K min}^{-1}$  using Weibull functions.

From the ratio of the peak areas for the separated first and second peaks, the contribution  $c$  of each peak to the overall reaction was determined as  $(c_1, c_2) = (0.52 \pm 0.02, 0.48 \pm 0.02)$ . The mathematically separated peaks at different  $\beta$  were used as the kinetic rate data (Figure S6).



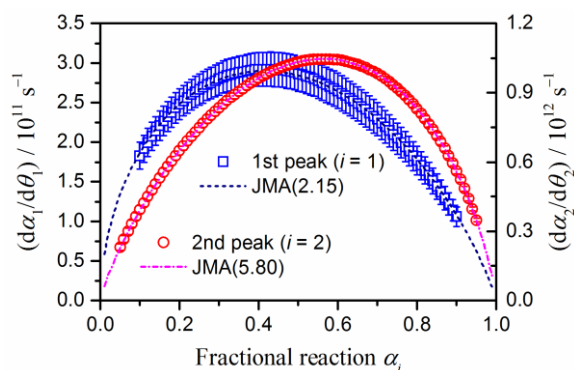
**Figure S6.** Kinetic rate data at different  $\beta$  derived from the mathematically separated DTG peaks: (a) first peak ( $i = 1$ ) and (b) second peak ( $i = 2$ ).

For both the first and second peaks, the kinetic rate data indicated systematic shifts to higher temperatures with increasing  $\beta$ . On the other hand, very different trends for the  $\alpha$ -dependent changes in the apparent activation energies ( $E_a$ ) determined by applying the Friedman method<sup>S7</sup> were found for the kinetic rate data of the separated first and second DTG peaks (Figure S7). For the first DTG peak, a systematic decrease in the  $E_a$  value during the course of the reaction was observed, while for the second DTG peak, a practically constant  $E_a$  value was obtained. The systematic change in the  $E_a$  value with  $\alpha$  observed for the first peak indicates that the isoconversional relationship failed because of the changes in the self-generated conditions as the reaction advanced and depending on  $\beta$ . In this situation, an average value for  $E_{a,1}$ ,  $109.1 \pm 20.8 \text{ kJ mol}^{-1}$  ( $0.1 \leq \alpha_1 \leq 0.9$ ), was tentatively used as the  $E_a$  value for the first peak. The average value for the practically constant  $E_{a,2}$  value for the second peak was  $115.5 \pm 1.3 \text{ kJ mol}^{-1}$  ( $0.05 \leq \alpha_2 \leq 0.95$ ). These  $E_a$  values are nearly coincident with one another and also in agreement with that determined for the overall reaction under isothermal and controlled rate conditions,  $112.5 \pm 1.2 \text{ kJ mol}^{-1}$  ( $0.05 \leq \alpha \leq 0.95$ ).



**Figure S7.**  $E_a$  values at different  $\alpha$  determined using the Friedman method for the separated first and second DTG peaks.

Using the respective  $E_a$  values, experimental master plots of  $(d\alpha/d\theta)$  versus  $\alpha$ <sup>S8-S14</sup> for the separated first and second DTG peaks were drawn (Figure S8) and satisfactorily fitted using the JMA( $m$ ) model<sup>S15-S18</sup> with  $m_1 = 2.15 \pm 0.01$  and  $m_2 = 5.80 \pm 0.01$ , respectively. The values for the preexponential factor  $A$  for the first and second peaks determined through nonlinear regression analysis for the fitting using the JMA( $m$ ) model were  $A_1 = (3.22 \pm 0.01) \times 10^{11} \text{ s}^{-1}$  and  $A_2 = (4.83 \pm 0.01) \times 10^{11} \text{ s}^{-1}$ , respectively.



**Figure S8.** Experimental master plots of  $(d\alpha/d\theta)$  versus  $\alpha$  for the separated first and second DTG peaks and fitting curves obtained using the JMA( $m$ ) model.

#### S4. Initial Kinetic Parameters for the Kinetic Deconvolution

The initial  $c_i$  values for the reaction under linear nonisothermal conditions were taken from those determined by the mathematical deconvolution. Because of the systematic decrease in the  $E_{a,1}$  values determined for the first DTG peak (Figure S7), the average  $E_a$  value determined for each separated peak was not employed for the initial values. Instead, considering the close agreement of both average  $E_{a,i}$  values for the separated DTG peaks with that determined for the reaction under isothermal and controlled conditions, the latter value of  $112.5 \text{ kJ mol}^{-1}$  was adopted for both reaction steps. The kinetic exponents  $m$  in the JMA( $m$ ) model for each reaction

step were set to 3.00 with expecting variation to a suitable value through the subsequent optimization run. After setting these kinetic parameters in Eq. 8 (see the main text), the order of the  $A_i$  values for each reaction step was determined by graphically comparing the result to the experimental kinetic curve. Table S1 summarizes the initial kinetic parameters used for the kinetic deconvolution analysis for the reaction under linear nonisothermal conditions.

**Table S1.** Initial kinetic parameters used for the kinetic deconvolution analysis of the thermal decomposition of SPC granules under linear nonisothermal conditions

Peak $i$	$c_i$	$E_{a,i} / \text{kJ mol}^{-1}$	$m_i$ in JMA( $m$ )	$A_i / \text{s}^{-1}$
1	0.52	112.5	3.00	$6.0 \times 10^{11}$
2	0.48	112.5	3.00	$3.0 \times 10^{11}$

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